

Mixture fraction measurements during the flame transmission at equipment of the type of protection “flameproof enclosure”

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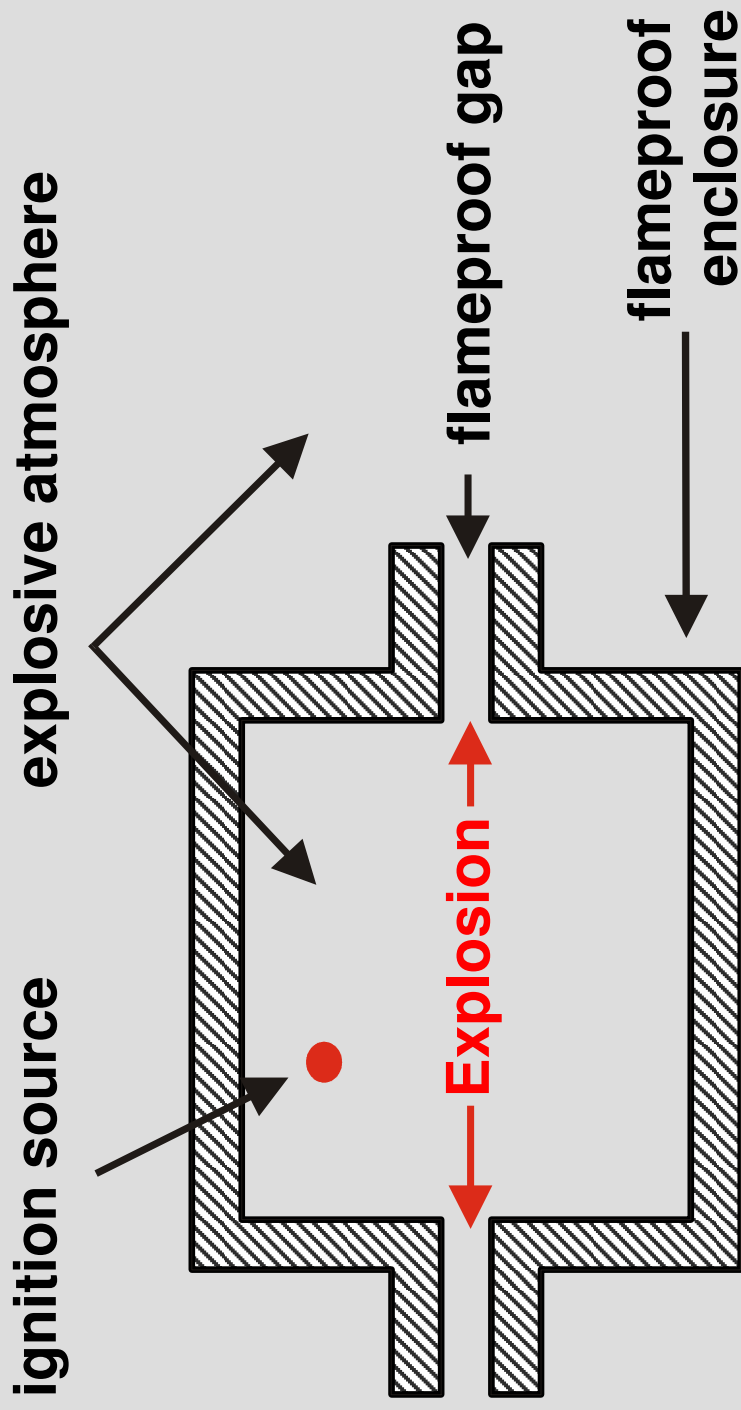


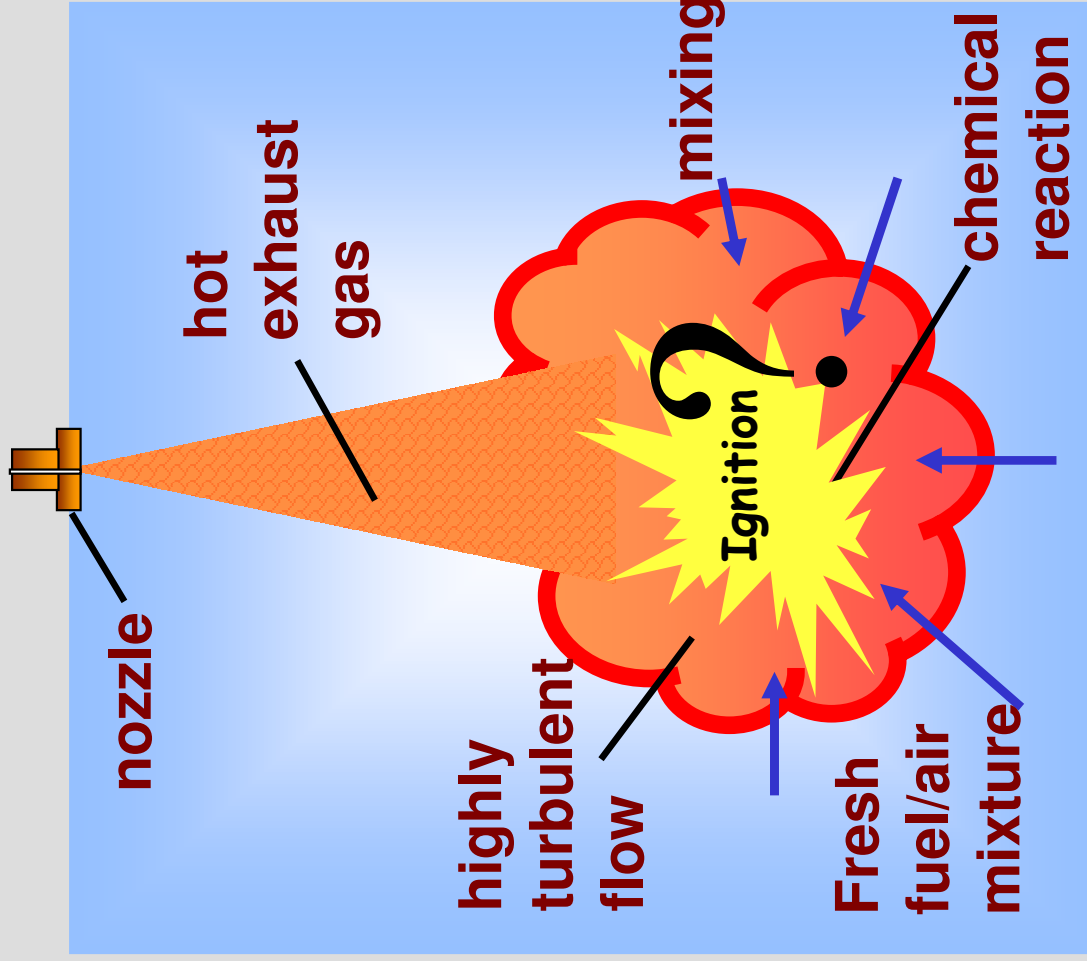
- Introduction
- Objectives
- Measurement Strategy
- Experimental Set-up
- Results
- Conclusions
- Outlook



IEC 60079-1: Test for non-transmission of an internal ignition

- Flameproof Enclosures





Influencing Factors

- Complex interaction between physical and chemical processes
- Competing influence of mixing, temperature and pressure on the ignition process
- Subsonic, sonic or supersonic flow regimes



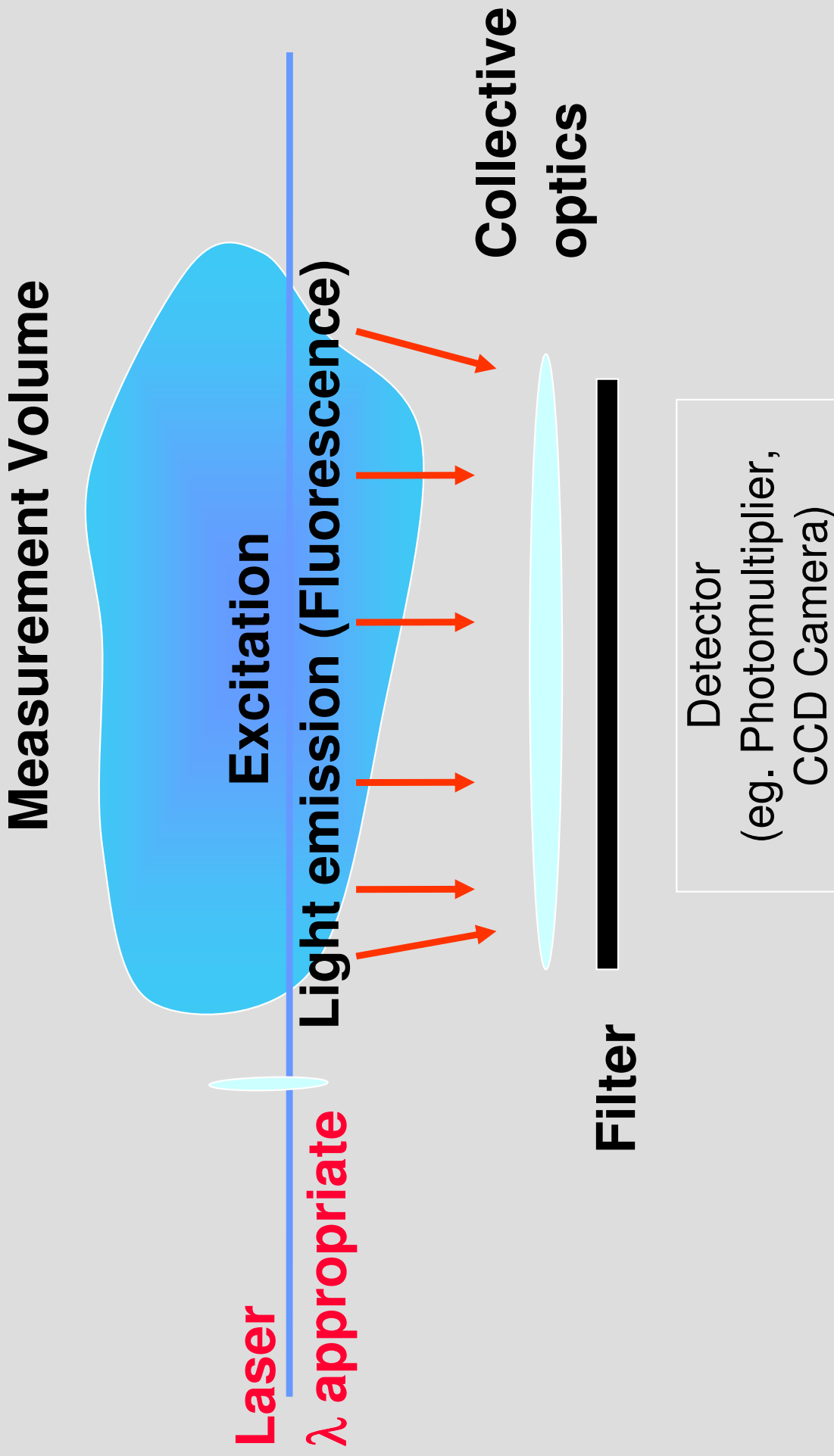
- Long term:
 - Develop a numerical model that can be used to predict hot jet ignition behaviour for a wide range of conditions.
- Short term:
 - Obtain empirical information about the mechanisms involved in the ignition process.
 - Use numerical simulations to guide the interpretation of the experimental results.

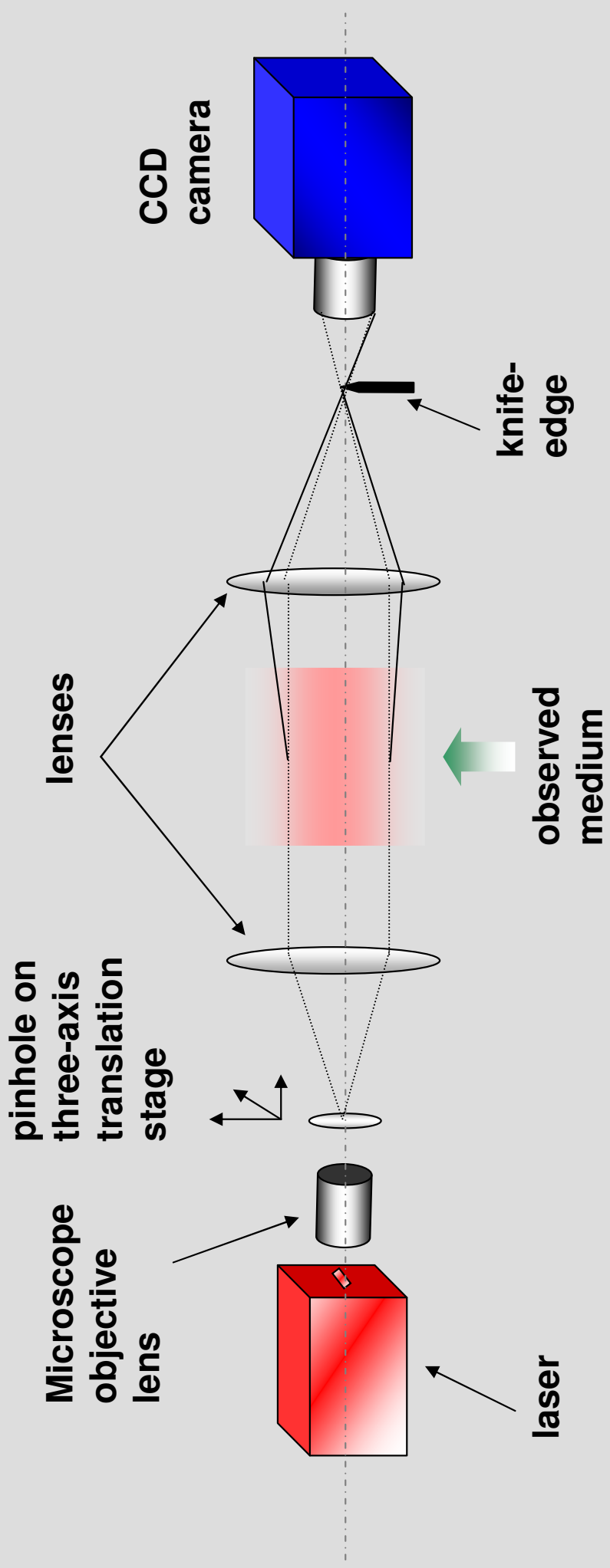


- Instationary and spatially inhomogeneous process
- Spatially and temporally resolved information
- Highly sensitive to disturbances
- Non-intrusive diagnostic method



- Study the temporal development of the jet structure
 - Use laser Schlieren visualisation
- Detect ignited regions inside the free jet flow
 - Visualise occurrence of OH radical (OH-LIF)
- Information about the instantaneous mixing between the hot burned gas and the cold unburned fuel/air mixture
 - Mixture fraction measurements using NO as tracer species (NO-LIF)





Requirements:

- simple, well-defined model
- optically accessible

First vessel:

Diameter = 60 mm

Length = 80 mm

Second vessel:

Volume = 12 dm³

Mixture composition :

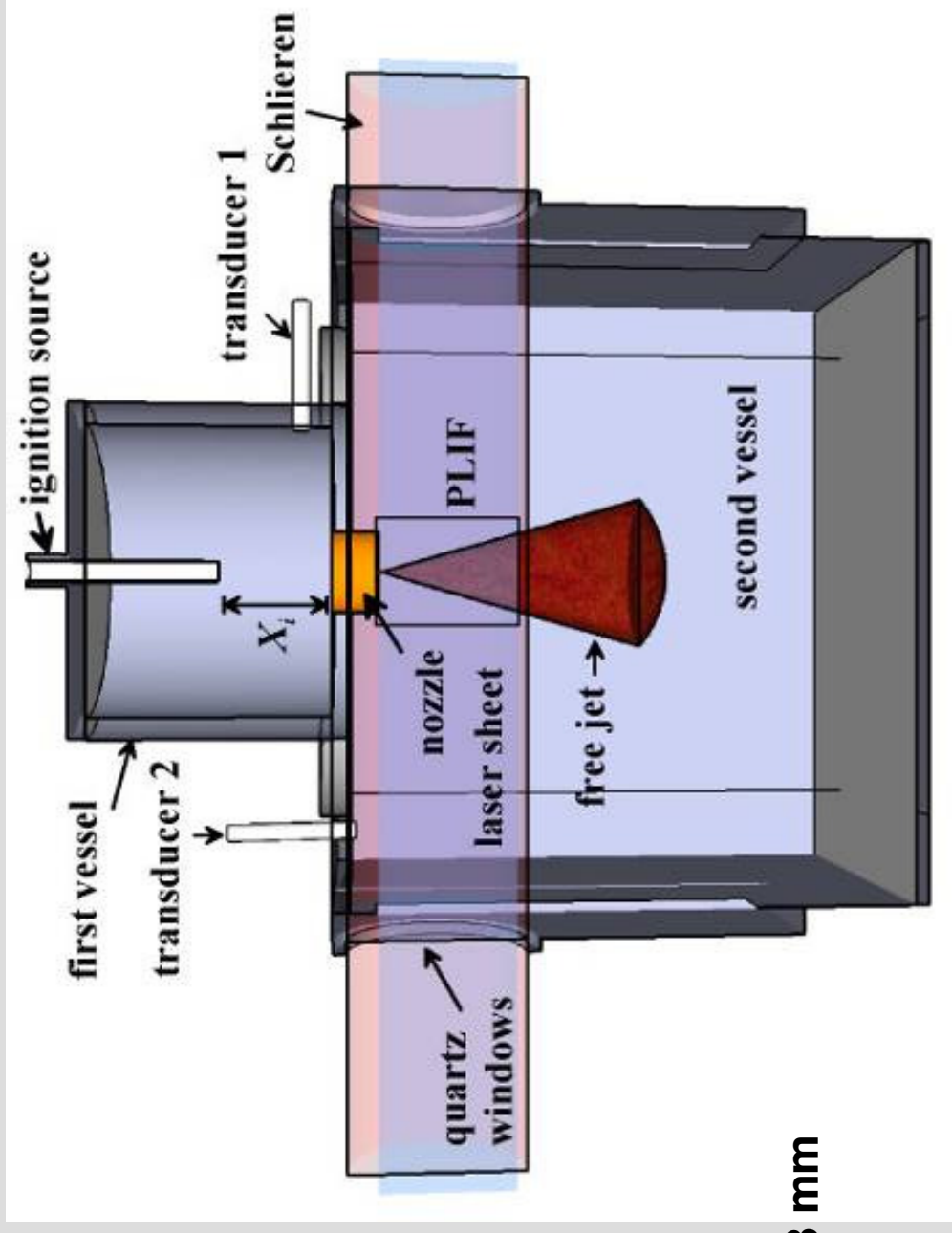
28% H₂ / 72 % Air

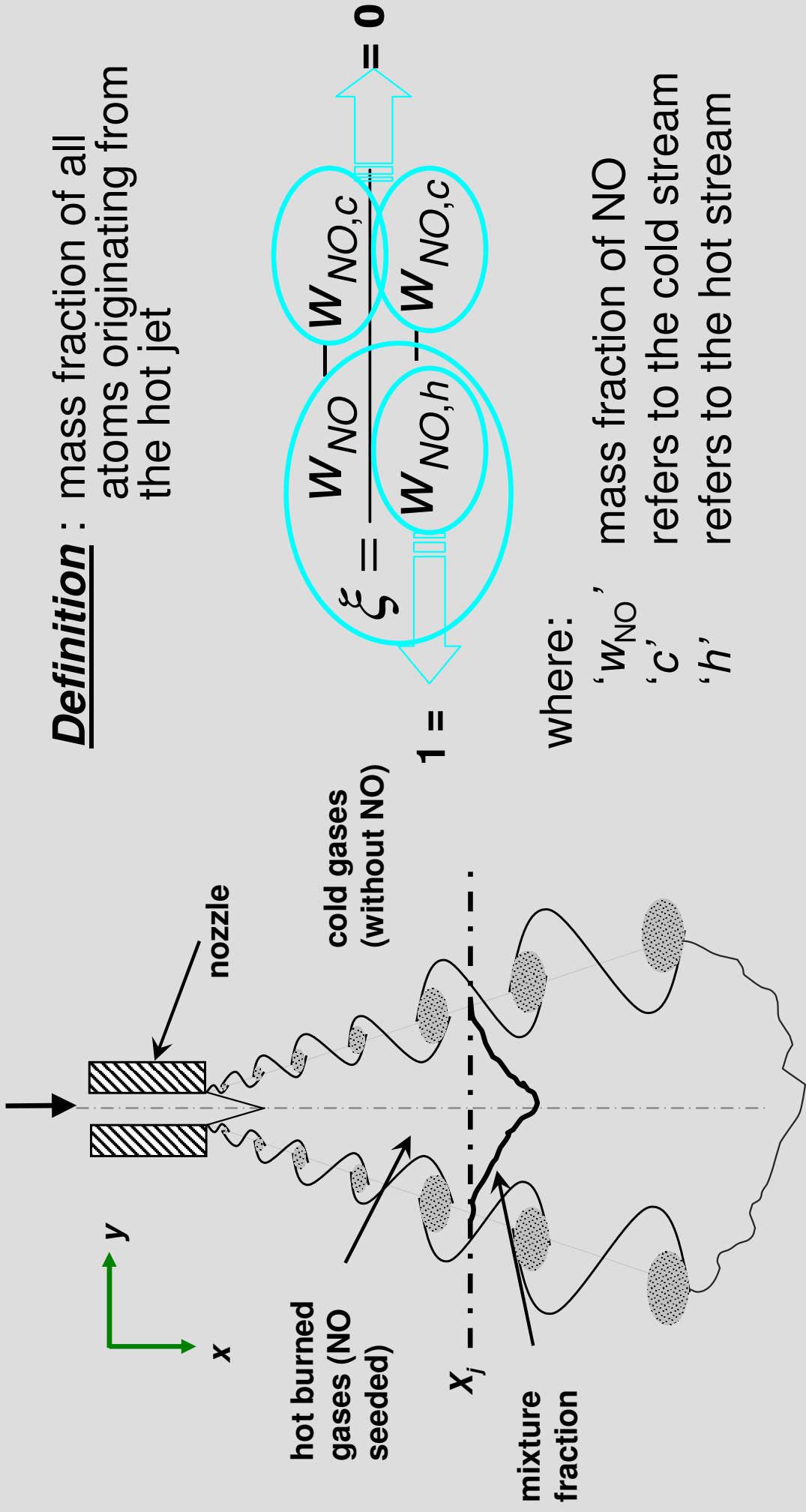
Nozzle:

Length = 25 mm

Diameter = 0.7–1.3 mm

$X_i = 24 - 56$ mm





Definition: mass fraction of all atoms originating from the hot jet

where:

- ' W_{NO} ' mass fraction of NO
- 'c' refers to the cold stream
- 'h' refers to the hot stream

Perform numerical simulations of the system to obtain a large database of realisable state vectors $\psi = (T, p, x)$ during the process of mixing and re-ignition

sp. Location	Pr	T	wNO	wN2	wO2	wH2O
0.00E+00	1.00E+05	1.20E+03	9.93E-04	7.35E-01	5.73E-01	2.51E-01
3.45E-04	1.00E+05	1.20E+03	9.90E-04	7.35E-01	1.24E-03	2.50E-01
6.90E-04	1.00E+05	1.19E+03	9.85E-04	7.35E-01	2.47E-03	2.48E-01
1.03E-03	1.00E+05	1.18E+03	9.76E-04	7.35E-01	4.51E-03	2.46E-01
1.38E-03	1.00E+05	1.17E+03	9.62E-04	7.35E-01	7.68E-03	2.43E-01
1.72E-03	1.00E+05	1.15E+03	9.41E-04	7.35E-01	1.23E-02	2.37E-01
2.07E-03	1.00E+05	1.13E+03	9.13E-04	7.34E-01	1.85E-02	2.30E-01
2.41E-03	1.00E+05	1.09E+03	8.78E-04	7.34E-01	2.64E-02	2.21E-01
2.76E-03	1.00E+05	1.05E+03	8.34E-04	7.34E-01	3.61E-02	2.10E-01
3.10E-03	1.00E+05	1.01E+03	7.84E-04	7.34E-01	4.74E-02	1.98E-01
3.45E-03	1.00E+05	9.58E+02	7.28E-04	7.34E-01	5.99E-02	1.84E-01
3.79E-03	1.00E+05	9.03E+02	6.67E-04	7.34E-01	7.34E-02	1.68E-01
4.14E-03	1.00E+05	8.46E+02	6.04E-04	7.34E-01	8.75E-02	1.52E-01
4.48E-03	1.00E+05	7.89E+02	5.41E-04	7.34E-01	1.02E-01	1.36E-01
4.83E-03	1.00E+05	7.32E+02	4.78E-04	7.33E-01	1.16E-01	1.21E-01



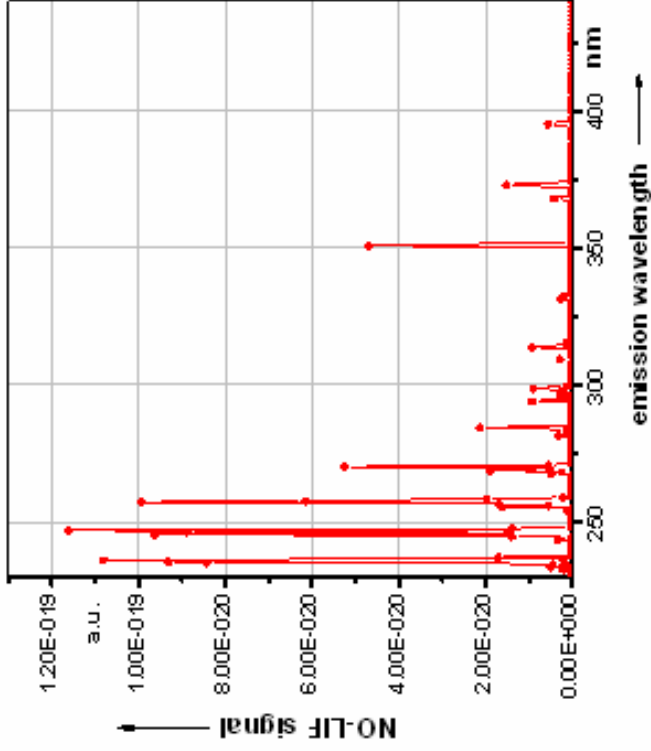
initial conditions:
 $800\text{K} < T_b < 1300\text{K}$
 $100\text{m/s} < v_b < 400\text{m/s}$

**interaction of hot burned
gas (NO seeded) with
unburned hydrogen/air
mixture**

**1D-Numerical
Simulations**

**Le = 1, no
gasdynamic effects,
adiabatic**

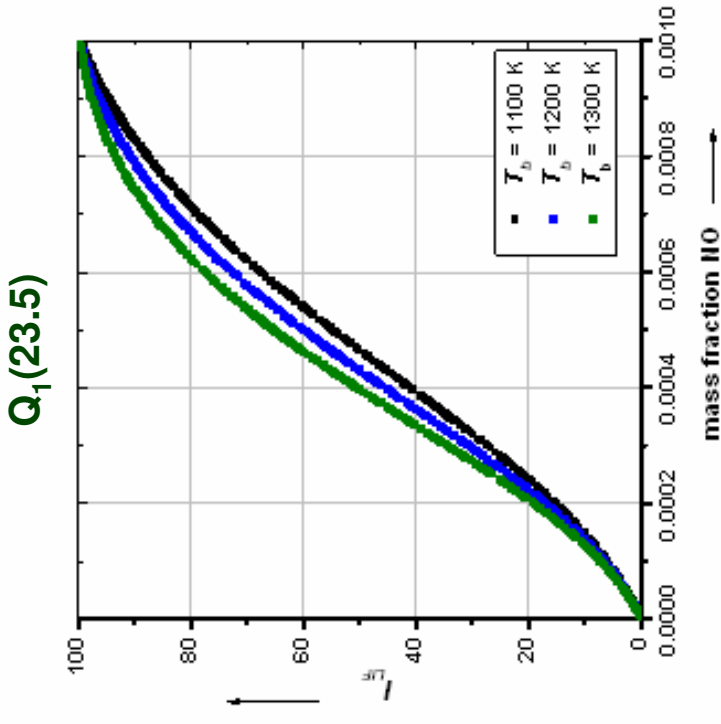
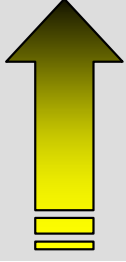
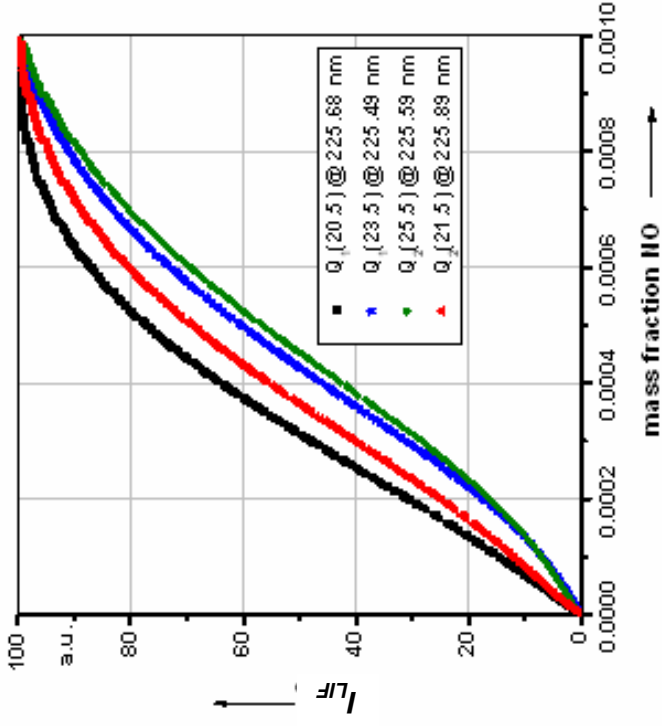
**H₂/air/NO reaction
mechanism, 160
elementary reactions, 19
species**



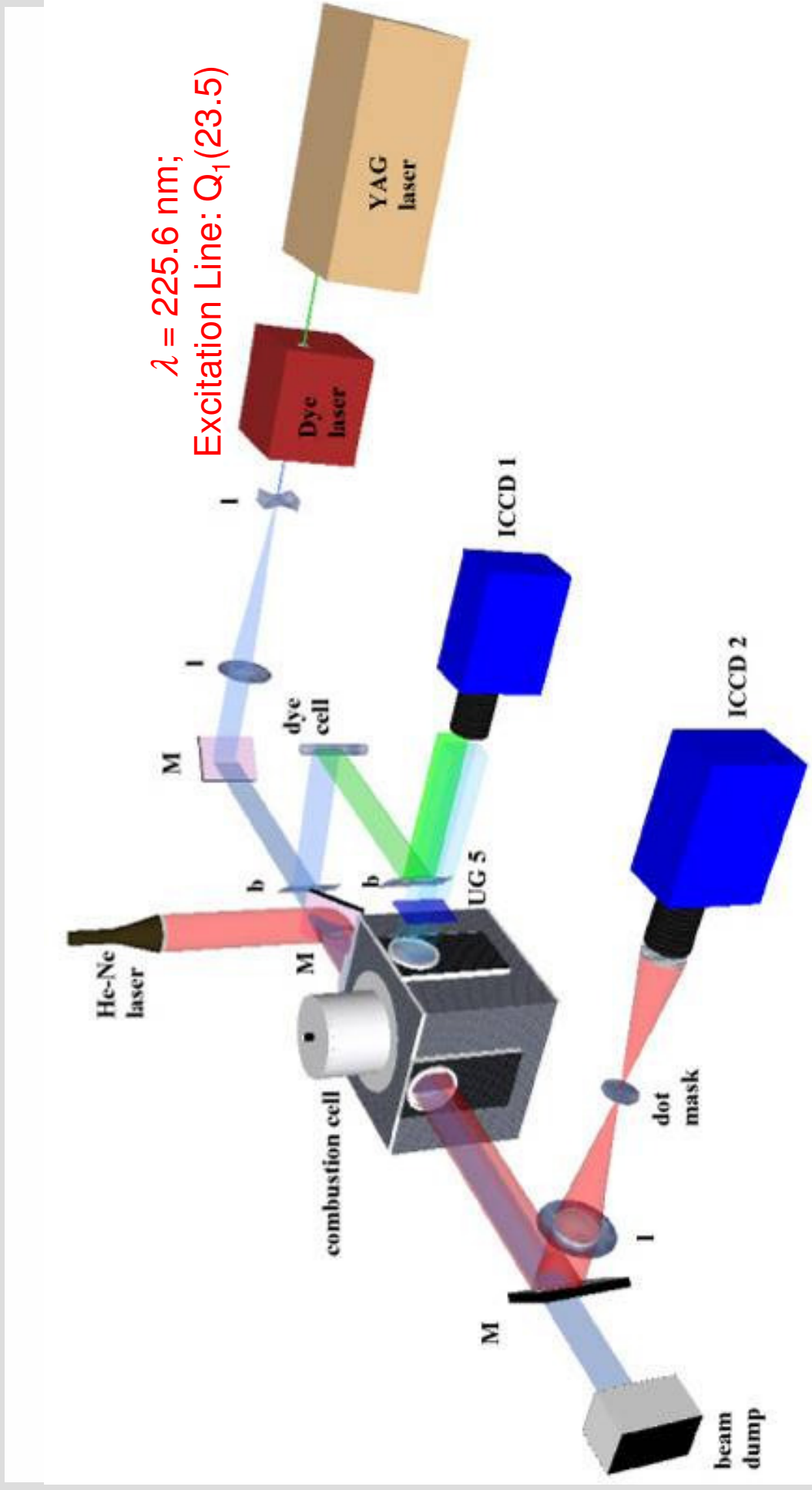
The state vectors so obtained are used for the spectroscopic simulation of corresponding NO-LIF-Signals using the program LIFSim*

$$S(T, p, x_i) = I_{\text{laser}} N_{\text{NO}} f_B(T) \sigma_{\text{eff}} \frac{A_{21}}{A_{21} + Q_{21}(T, p, x_i)}$$

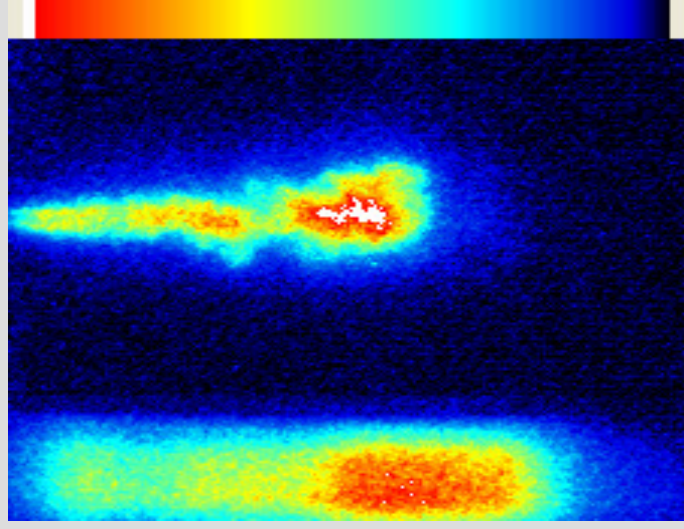
*W.G. Bessler, C. Schulz, V. Sick and J. Daily: A versatile modelling tool for nitric oxide LIF spectra. Proceedings of the Third Joint Meeting of the U.S. Sections of the Combustion Institute (2003) D33 1-6.



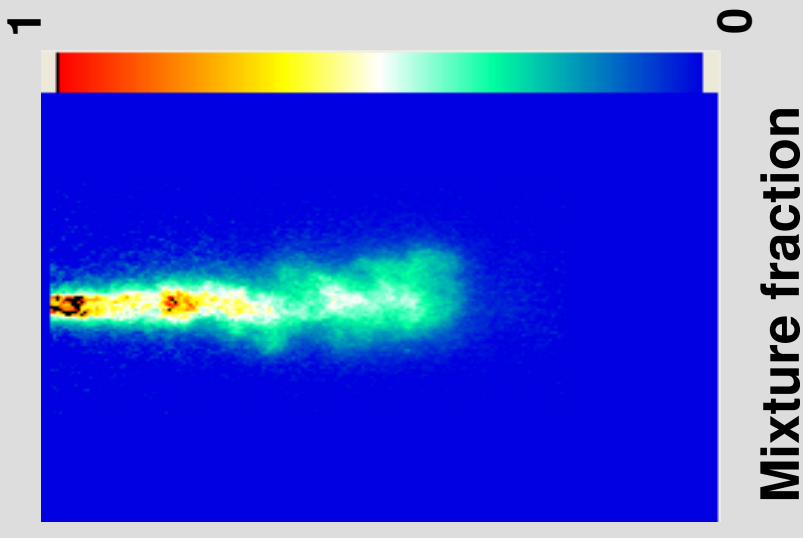
**Experiments performed using
excitation scheme with sharp
correlations between I_{LIF} and
NO mass fraction**



NO-LIF images converted to mixture fraction maps using the computed correlations



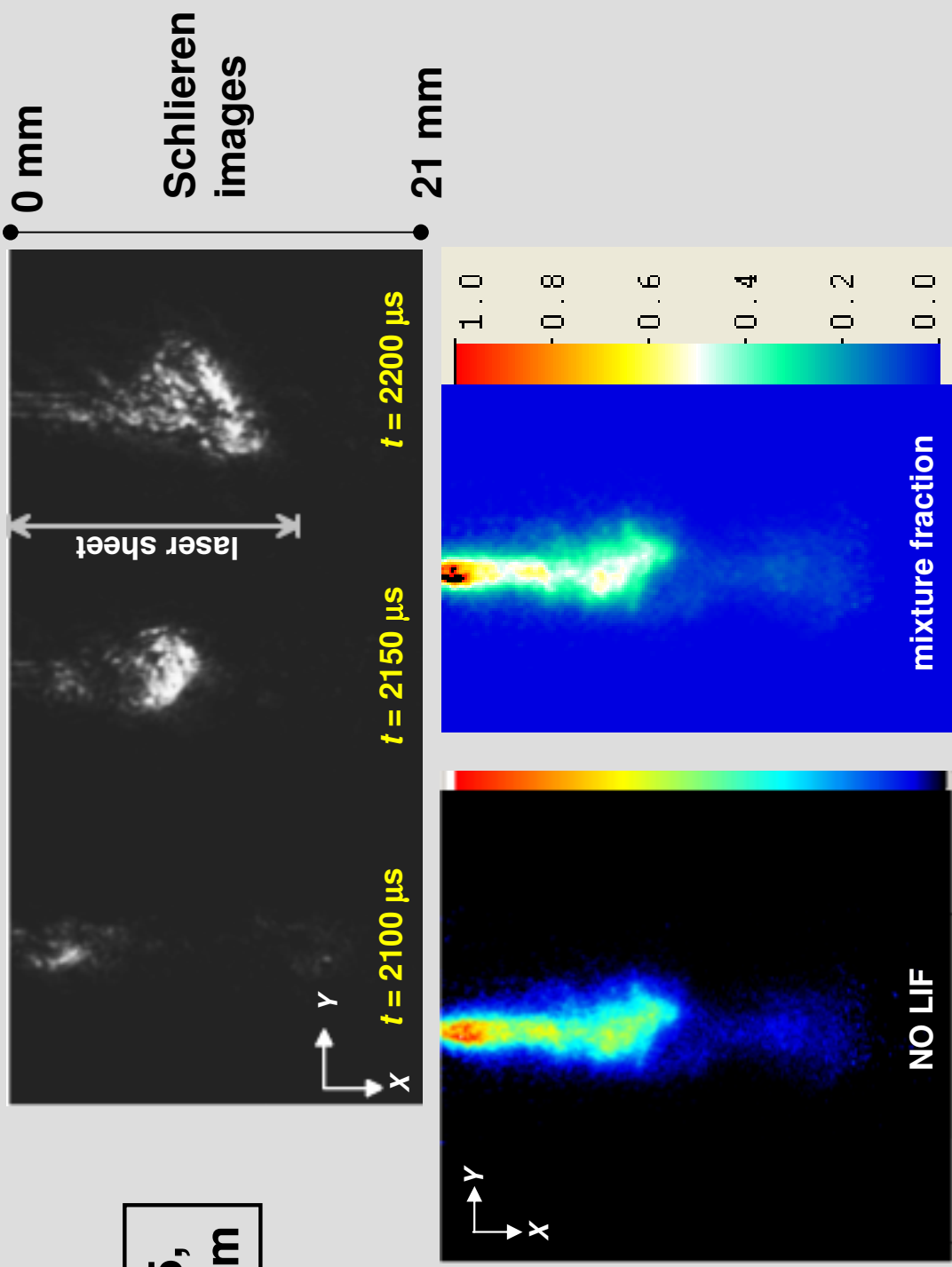
- Background noise corrections
- Laser sheet profile corrections
- Conversion to mixture fraction maps using correlations





$$p_1/p_2 = 1.5,$$

$$d = 0.7 \text{ mm}$$

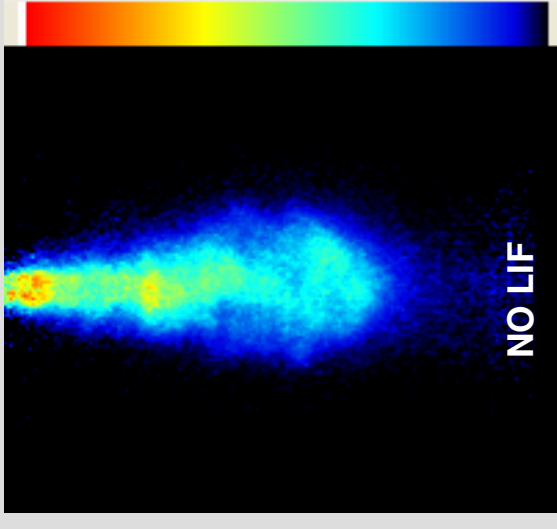
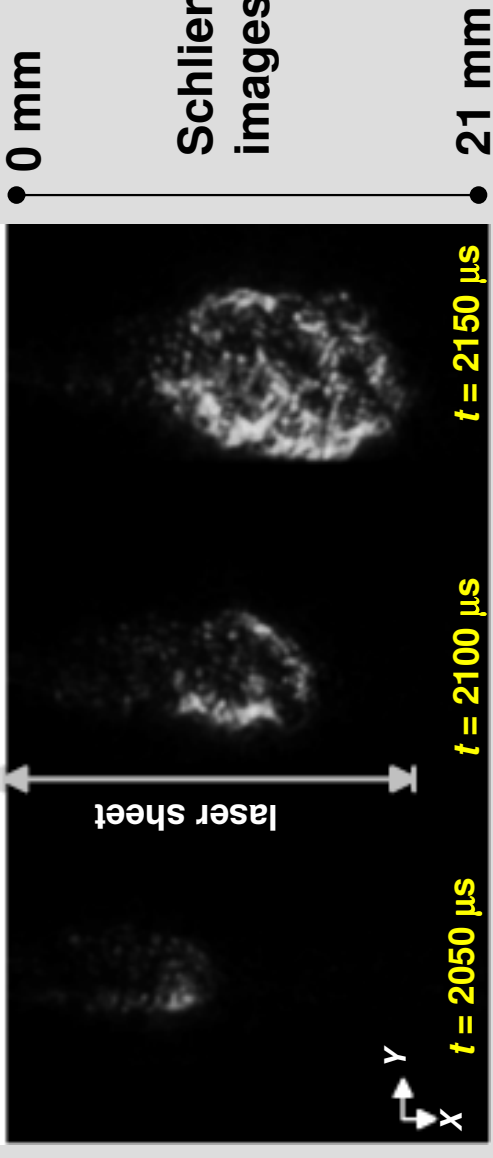


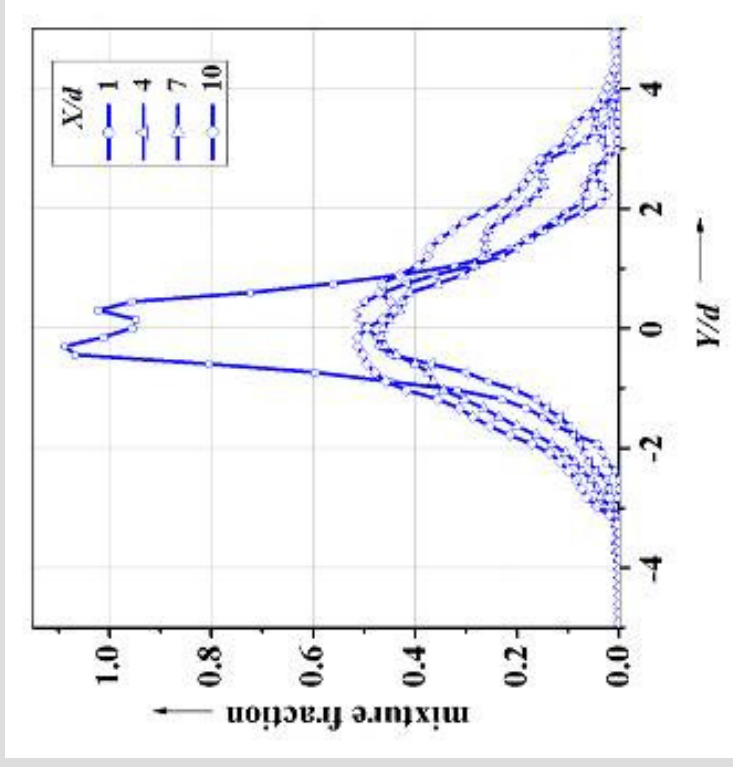
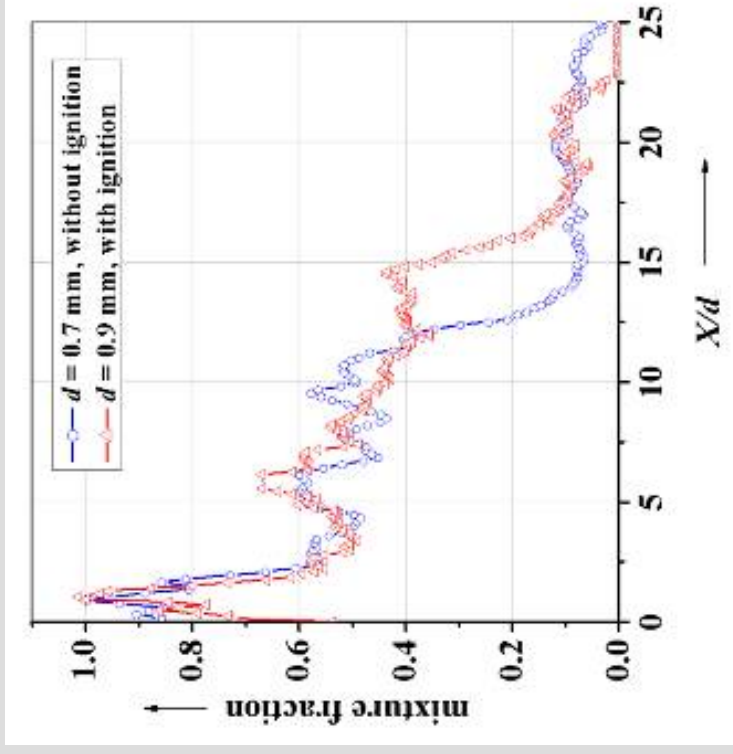
Case 2: With ignition



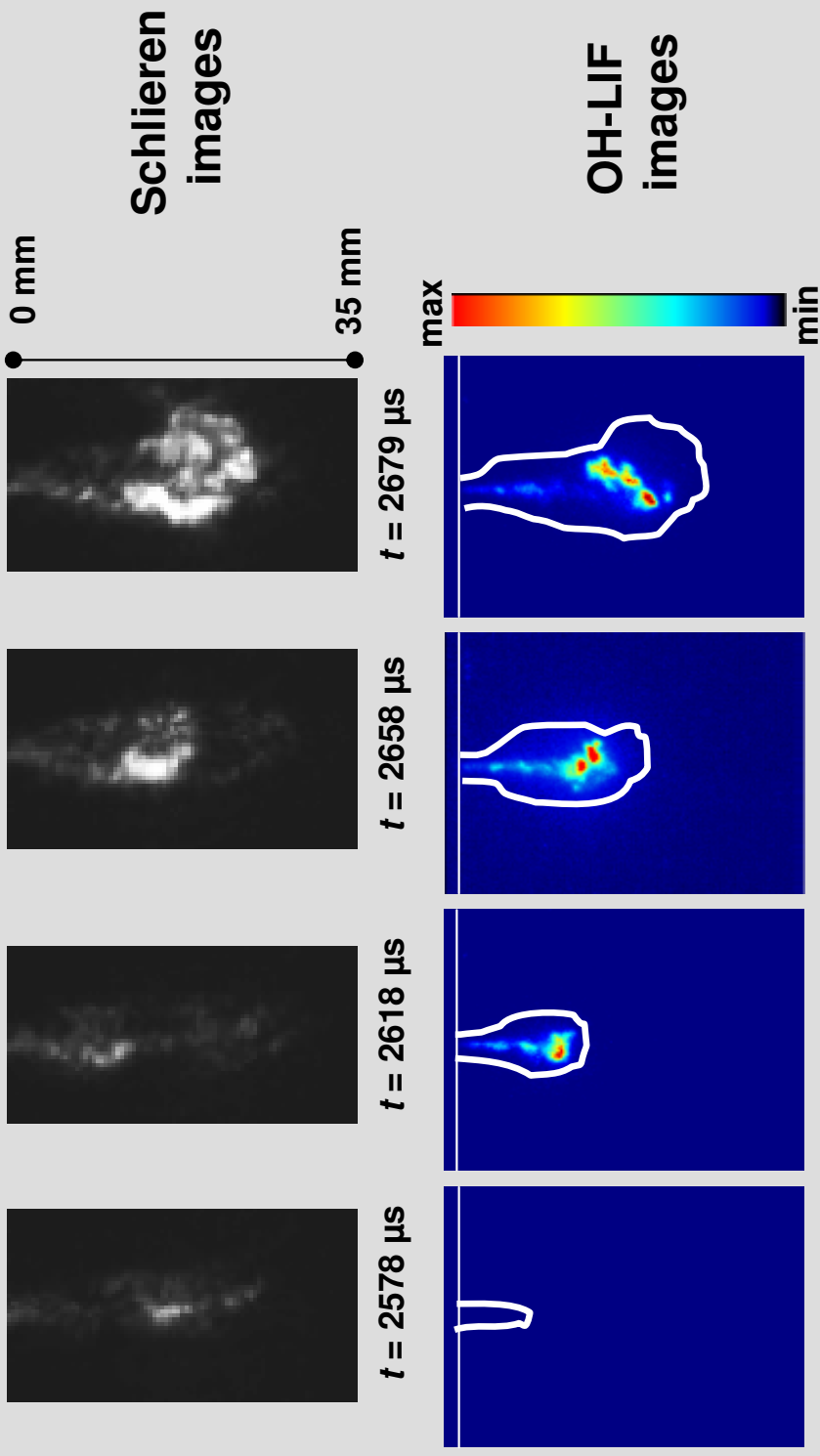
$$p_1/p_2 = 1.44,$$

$$d = 0.9 \text{ mm}$$





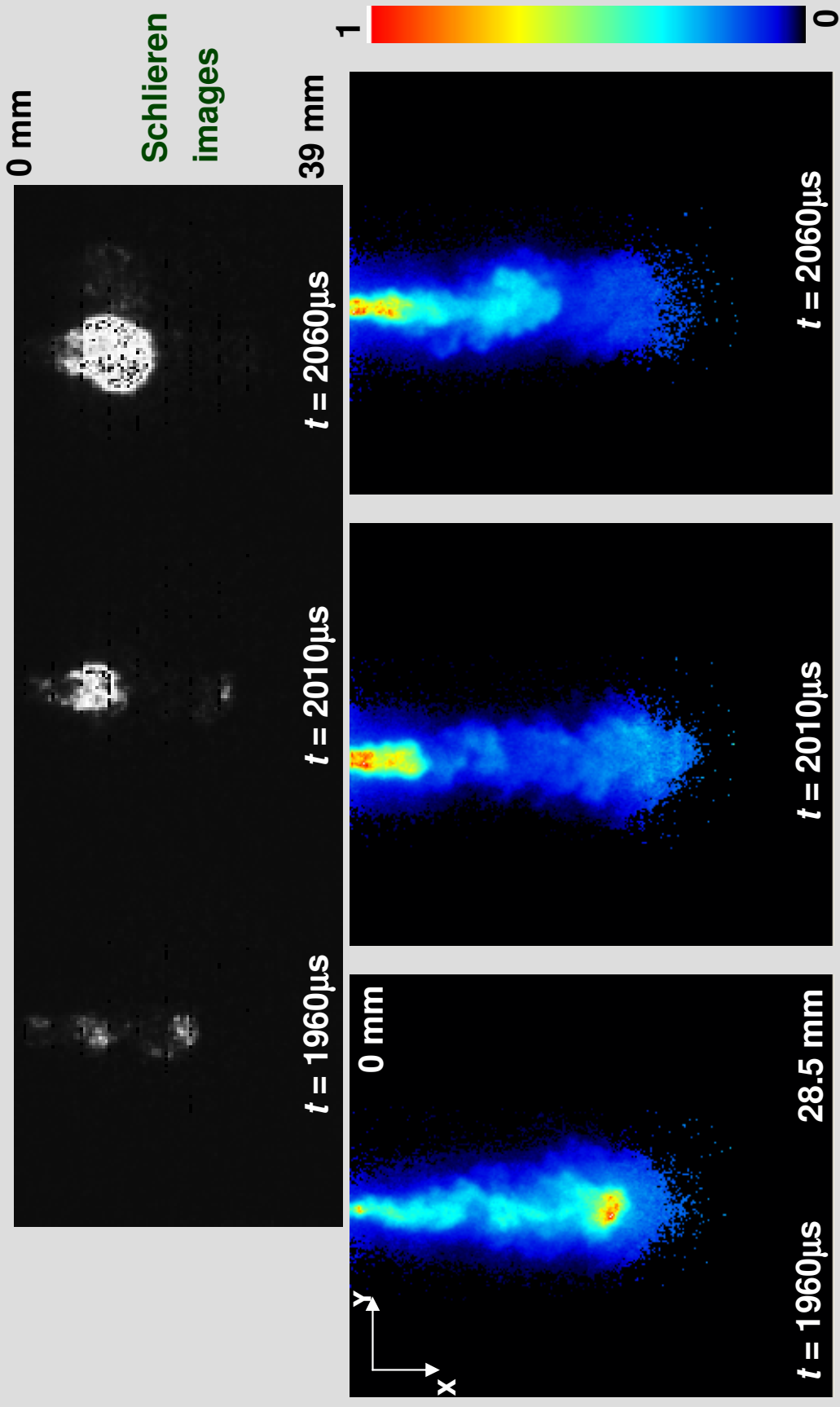
- The axial profile shows a rapid decrease with downstream distance, indicative of the hot jet/unburned gas mixing
- The radial profile shows a progressive decay from the center value of the jet to the border, indicative of the rapid entrainment and turbulent mixing of the cold unburned mixture with the hot product jet



$p_1/p_2 = 2.06$, $d = 1.0 \text{ mm}$

Sadanandan, R. et al.: Proceedings of the Combustion Institute (2006) 31 719-726

$$X_i = 24 \text{ mm}, p_1/p_2 = 1.44, d = 0.8 \text{ mm}$$





- A novel measurement method has been developed for the instantaneous, quantitative, 2D and spatially resolved measurement of mixture fraction maps.
- The method is based on numerical simulations and spectroscopic modeling.
- Computed correlations between NO mass fractions and LIF signals are used to deduce mixture fraction profiles from NO-LIF images.
- Quantitative, planar instantaneous mixture fraction maps during the ignition of hydrogen/air mixtures by hot jets can be obtained.
- The method is applicable in cases where ignition and subsequent combustion has not raised the temperature to too high levels (< 1300 K).
- An alternative excitation scheme or a simultaneous second measurement is necessary to include those cases.